

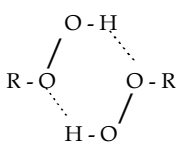
	<u>Page</u>	<u>Equation</u>	<u>Error</u>	<u>Correction</u>
<u>Tuma / Bagner</u>				
1.	28	2	$\Delta T$	1000
<u>Fauske</u>				
2.	55	1 <sup>st</sup> line	with =	with $\dot{P}$ =
3.	55	2 <sup>nd</sup> line	in =	in $\dot{Q}_g$ =
4.	56	4 <sup>th</sup> line	$\rho_o$	$\rho_{o2}$
5.	56	3	$M$	$m$
6.	56	4	$Q_T$	$\dot{Q}_T$
7.	56	4	$Q_D$	$C_D$
8.	56	5	$Q_D$	$C_D$
9.	58	4 <sup>th</sup> line	in illustrating	in Figure 5 illustrating
10.	58	9 <sup>th</sup> line	with =	with $\dot{T}$ =
11.	59	31 <sup>st</sup> line	, =	, $\dot{T} = 0.4$
12.	60	12	$\rho$	$m$
<u>Leung</u>				
13.	122	Figure 16	Figure 16	Figure 17. Self-Heat Rate Data for BPO Decomposition from 19 RSST Runs.
14.	123	Figure 17	Figure 17	Figure 16. Self-Heat Rate Data for BPO Decomposition from 7 VSP Runs.
15.	128	14 <sup>th</sup> line	throughput	delete

	<u>Page</u>	<u>Equation</u>	<u>Error</u>	<u>Correction</u>
16.	128	15 <sup>th</sup> line	rate.	rate throughout.
17.	133	16 <sup>th</sup> line	to, a	to a
<u>Gustin</u>				
18.	186	Figure 7	Dewar Test 5. Heat-rate curve.	Dewar Test 5. Pressure corrected for the nitrogen pad gas versus temperature.
19.	187	Figure 8	-	Dewar Test 5. Heat-rate curve.
20.	191	2 <sup>nd</sup> equation	$TO$	$T_o$
21.	192	2 equations	$\frac{\quad}{\quad}$	$\frac{\quad}{\quad^2}$
22.	194	2 <sup>nd</sup> equation	$e^{-E/RT}$	$e^{E/RT}$
23.	194	5 <sup>th</sup> equation	$e^{-Ed/RT}$	$e^{Ed/RT}$
24.	197	21 <sup>st</sup> line	thermal initial	thermal inertia
<u>Hawksworth and Ladlow</u>				
25.	210	Table 1	9	7.9
26.	216	first 2 equations	$A_{ws}^{0.556}$	$A_{ws}^{0.566}$
<u>Grolmes</u>				
27.	221	1	$K =$	$k =$
28.	226	Table 2, Footnote	$P = 950$	$\rho = 950$
29.	228	10b	$W$	$w$
30.	232	26	$\underline{m_o}(\underline{\quad})$	$\underline{x_o m_o}(\underline{\quad})$

	<u>Page</u>	<u>Equation</u>	<u>Error</u>	<u>Correction</u>
31.	233	27 and 29a	$\frac{N_{\text{gmr}} R}{V}$	$\frac{n_{\text{gmr}} R}{V}$
32.	233	31	$I_{\text{TEVT}} =$	$I_{\text{TEVT}} \approx$
33.	234	33	$m_o$	-
34.	234	34	$\frac{C_d A}{m_o} \approx$	$\frac{C_d A}{m_o} =$
35.	239	Table 5, Title	$x = 0.40$	$x = 0.50$

Duh, et al.

36. Caution: Discussions subsequent to presentation of this paper revealed that a copper test cell was used to obtain the data. CHP is very susceptible to metal-induced surface reactions. The data possibly represent a thermally-induced decomposition. A copper-induced (acid-catalyzed) cleavage reaction is indicated by the presence of phenol as one of the decomposition products. This information was not considered during preparation of the paper.

37.	252	1.1	-	$2 \text{ ROOH} \Leftrightarrow [\text{ROOH}]_2$
38.	252	1.2	-	
39.	260	Between a.5 and a.6	-	Combining equations (a.2), (a.4) and (a.5)

Leung

40.	319	17 <sup>th</sup> line	fluid density ( $p$ )	fluid density ( $\rho$ )
41.	319	17 <sup>th</sup> line	$v = 1/p$	$v = 1/\rho$
42.	320	3	$\int$	$\int$

	<u>Page</u>	<u>Equation</u>	<u>Error</u>	<u>Correction</u>
43.	320	8 <sup>th</sup> line	where the $A$ parameter	where the $\omega$ parameter
44.	320	15 <sup>th</sup> line	on the $A$ value,	on the $\omega$ value,
45.	321	4 <sup>th</sup> line	an enthalpic flash	an isenthalpic flash
46.	321	8	$\frac{G}{\sqrt{P_o/\rho_o}}$	$\frac{G}{\sqrt{P_o \rho_o}}$
47.	321	9	$(\omega^2 - 2\omega)\left(\frac{1-P_c}{P_o}\right)$	$(\omega^2 - 2\omega)\left(\frac{1-P_c}{P_o}\right)^2$
48.	321	10	$\frac{G}{\sqrt{P_o/v_o}}$	$\frac{G_c}{\sqrt{P_o/v_o}}$
49.	322	13	$\frac{G}{\sqrt{P_o \rho_{go}}}$	$\frac{G_c}{\sqrt{P_o \rho_{go}}}$
50.	322	14	$\frac{G}{\sqrt{P_o \rho_{go}}}$	$\frac{G}{\sqrt{P_o \rho_{go}}}$
51.	324	17 <sup>th</sup> line	(or $L \cos l$ )	(or $L \cos \theta$ )
52.	324	18 <sup>th</sup> line	$G^* \equiv$	$G^* =$
53.	325	18	$G =$	$G^* =$
54.	324	14 <sup>th</sup> line	and $A$ .	and $\omega$ .
55.	325	21	$-\int_{\eta_2}^{\eta_1}$	$-\int_{\eta_1}^{\eta_2}$
56.	325	21	)	) $d\eta$
57.	326	10 <sup>th</sup> line	and $A$ .	And $\omega$ .
58.	329	6 <sup>th</sup> line	the $A$ parameter	the $\omega$ parameter
59.	337	18 <sup>th</sup> line	$\eta_i \equiv$	$\eta_i =$

	<u>Page</u>	<u>Equation</u>	<u>Error</u>	<u>Correction</u>
60.	337	19 <sup>th</sup> line	$\eta_2 =$	$\eta_2 =$
61.	341	39	$c^* = \frac{C}{\sqrt{Pv}} =$	$c^* = \frac{c}{\sqrt{Pv}} =$
62.	342	4 <sup>th</sup> line	by the $A$	by the $\omega$
63.	342	7 <sup>th</sup> line	The present $A$	The present $\omega$
64.	345	7 <sup>th</sup> .line	with $A$ ,	with $\omega$ ,
65.	347	11 <sup>th</sup> line	lb <sub>f</sub> was	lb <sub>f</sub> was
66.	347	13 <sup>th</sup> line	an $A$ value	an $\omega$ value
67.	351	7 <sup>th</sup> line	Since $G\sqrt{P_o \rho_o}$	Since $G / \sqrt{P_o \rho_o}$
68.	351	last equation	$\left(\frac{m^3/kg}{J/kg}\right)$	$\left(\frac{m^3/kg}{J/kg}\right)^2$
<u>Fauske</u>				
69.	353	1	— ]	— ] <sup>-1/2</sup>
70.	354	2 <sup>nd</sup> line	$G_{x_o=0}^2$	$G_{x_o=0}$
71.	354	11 <sup>th</sup> line	$G_{x_o=1}^2$	$G_{x_o=1}$
72.	354	17 <sup>th</sup> line	flows, is	flows, $G_{x_o=0}$ is
73.	354	20 <sup>th</sup> line	flows is	flows $G_{x_o=1}$ is
74.	355	6 <sup>th</sup> line	water, flows can	flows $G_{x_o=0}$ can be
75.	355	5	$(T_o - C_o)^{-1/2}$	$(T_o C_o)^{-1/2}$
76.	355	11 <sup>th</sup> line	not effect the	not affect the
77.	355	18 <sup>th</sup> line	and is again	and $G_{x_o=1}$ is again

	<u>Page</u>	<u>Equation</u>	<u>Error</u>	<u>Correction</u>
78.	355	22 <sup>nd</sup> line	$(L < 0.1 \text{ m})$	$(L > 0.1 \text{ m})$
79.	355	23 <sup>rd</sup> line	Equation (9)	Equation (8)
<u>Darby</u>				
80.	371	8	$(1-\eta)^{\frac{k-1}{k}}$	$(1-\eta^{\frac{k-1}{k}})$
81.	373	11	$\eta_c = \left[ \frac{1 - \beta^4 \eta^{\frac{2}{k}}}{\frac{k+1}{2} + \beta^4 \eta^{\frac{2}{k}} \left( \eta^{\frac{1-k}{k}} - \frac{k+3}{2} \right)} \right]^{\frac{k}{k-1}}$	
82.	373	15 <sup>th</sup> line	$0.528 < \eta_c < 0.656$	$0.528 < \eta_c < 0.497$
83.	373	16 <sup>th</sup> -21 <sup>st</sup> lines	The . . .out.	Delete
84.	376	12	$X = \frac{S_{Lo} - S_{L0}}{S_{LG}} =$	$X =$
85.	376	13	$v = v_G + v_L (1 - x)$	$v = v_G x + v_L (1 - x)$
86.	378	21	$\bar{\}$	$\bar{\}_t$
87.	381	Table 1	$\rho_L = c_0 + P + c_2 + P^2$	$\rho_L = c_0 + c_1 P + c_2 P^2$
88.	382	22	$\left( \frac{G_o v_o}{v_n} \right)$	$\left( \frac{G_o v_o}{v_n} \right)^2$
89.	383	27	$\underline{\omega \ln \eta = (\omega - 1)}$	$\underline{\omega \ln \eta + (\omega - 1)}$
90.	383	30	$= \sqrt{\left( \frac{\partial P}{\partial \rho} \right)_s}$	$= \sqrt{\left( \frac{\partial P}{\partial v} \right)_s}$
91.	387	18 <sup>th</sup> line	of 1/3 or 1/3.	of 1/3 or 1/2.

	<u>Page</u>	<u>Equation</u>	<u>Error</u>	<u>Correction</u>
92.	387	40	41	40
93.	388	41	$\left(\frac{\rho_L}{\rho_G}\right)^{(a_2-1)}$	$\left(\frac{\rho_L}{\rho_G}\right)^{(a_2+1)}$
94.	391	15 <sup>th</sup> line	in Eqs. (42)-(43).	in Eqs. (43)-(44).
95.	391	19 <sup>th</sup> line	of Eqs. (47) and (48)	of Eq. (48) (e.g.
96.	392 and 393	Table 3	Subcooled $L \leq 10$ cm: $N_{NE} = 1$ $L > 10$ cm, $N_{NE}$	Subcooled $L \leq 10$ cm: $N_{NE}$ $L > 10$ cm, $N_{NE} = 1$
97.	394	NOTATION	-	$d$ nozzle diameter
98.	394	NOTATION	$G^* = \sqrt{G / (P_o \rho_{Lo})}$	$G^* = G / \sqrt{(P_o \rho_{Lo})}$
99.	395	Subscripts	-	o vessel (stagnation) conditions

Melhem

100.	432	5	$\underline{\Delta T C_p V \rho}$	$\underline{\Delta T C_p}$
101.	433	7	$\overline{V_v - V_1}$	$\overline{(V_v - V_1)}$
102.	433	10	$A$ in (m <sup>2</sup> /1000 kg)	$A$ (m <sup>2</sup> /1000 kg)
103.	435	18 <sup>th</sup> line	$= 0$ and $\alpha =$	$= 0$ and $\alpha =$
104.	435	21 <sup>st</sup> line	of $P = P_o$ to	of $P/P_o$ to
105.	447/448 (three places)/ 449	equations	k (ft <sup>3</sup> /lb mole hr)	k (lb mole/ft <sup>3</sup> hr)

Page                      Equation                      Error                      Correction

106.	450	28 <sup>th</sup> line	literature half-life information	literature information
107.	450	1 <sup>st</sup> equation	$9.4672 \text{ E}+ 19 \exp(-62000)$	$1.0186 \text{ E}+ 9 \exp(-27675)$
108.	453	11 <sup>th</sup> line	(Figure 4) (Figure 5)	(Figure 5) (Figure 6)
109.	453	12 <sup>th</sup> line	(Figure 6) (Figure 7)	(Figure 7) (Figure 8)
<u>Shaw</u>				
110.	475	Table 7	2,5057	25,057
111.	479	Table 13	Benchmark 8	Benchmark 9
<u>Sheu, et al.</u>				
112.	573	9	$\frac{\partial}{\text{Pr}} \exp[-]$	$\frac{\delta}{\text{Pr}} \exp[-]$
<u>Hesse</u>				
113.	587	1 <sup>st</sup> three equations	replace	$h_1 = R \left[ 1 + 2 \cos\left(\frac{\phi}{3}\right) \right]$ $h_2 = R \left[ 1 - 2 \cos\left(\frac{\phi}{3} + \frac{\pi}{3}\right) \right]$ $h_3 = R \left[ 1 - 2 \cos\left(\frac{\phi}{3} - \frac{\pi}{3}\right) \right]$
114.	587	6 <sup>th</sup> line	where $\varphi$ satisfies	where $R$ is the vessel radius, $C_f \geq 0.5$ , and $\varphi$ satisfies
115.	587	9 <sup>th</sup> line	range (0, 2R) and	range (0, R) and



	<u>Page</u>	<u>Equation</u>	<u>Error</u>	<u>Correction</u>
116.	587	9 <sup>th</sup> line	-	by the mensuration formula $A_{CR} = \frac{\pi}{3} \left[ \frac{6}{\pi h} (1 - C_f) V - h \right]$
117.	598	3 <sup>rd</sup> equation	$\rho g \cos \beta +$	$\rho g +$
118.	600	2 <sup>nd</sup> equation	$k_v^3 (\rho_1 - \rho_v)$	$k_v^3 \rho_v (\rho_1 - \rho_v)$
119.	601	3 <sup>rd</sup> equation	$\left( \frac{c_p \Delta T_x}{h_{fg}} \right)$	$\left( \frac{c_p \Delta T_x}{h_{fg}} \right)^{1/5}$
120.	602	1 <sup>st</sup> equation	$T_{oo}$	$T_{oo}'$
121.	602	1 <sup>st</sup> equation	$\frac{2k}{c\rho \Delta x^2}$	$\frac{2k \Delta \phi}{c\rho \Delta x^2}$
122.	602	1 <sup>st</sup> equation	$q'_{wall}$	$q^*_{wall}$
123.	603	10 <sup>th</sup> sentence	Forrest (1985)	Forrest (1995)
124.	611	1 <sup>st</sup> equation	$e^{1\Gamma}$	$e^{-\Gamma}$
<u>Leung</u>				
125.	619	1	$\left( \frac{v h_{fg}}{m_o u_{fg}} \right)^{1/2}$	$\left( \frac{V h_{fg}}{m_o u_{fg}} \right)^{1/2}$
126.	624	5	$- ]$	$- ]^{1/2}$
127.	625	Figure 10	9.	5.
128.	629	equation	$\frac{0.864 \text{ in}^2}{5 \text{ gal}}$	$\frac{0.864 \text{ in}^2}{3.26 \text{ gal}}$

	<u>Page</u>	<u>Equation</u>	<u>Error</u>	<u>Correction</u>
<u>Nichols</u>				
129.	675	reference 29	Lewis, B. and	29. Lewis, B. and
<u>Huang</u>				
130.	678	12 <sup>th</sup> line	( $\pm 15\%$	$\pm 15\%$
131.	693	2 <sup>nd</sup> line	divide ( $H$ into	divide $\Delta H$ into
132.	693	5 <sup>th</sup> line	( $S_c^* = 2$ )	( $S_c = 2$ )